

CONCRETE DESIGN ACCORDING TO EUROCODE 2 **(referred to the NATIONAL ANNEX for GERMANY)**

INTRODUCTION

Name: [REGBEM v 2.5](#)

The following program determines for a rectangular concrete beam the reinforcement both on top (**As2** on compressive side) and at the bottom (tensile area **As1**, see fig. 1), if the dimensions, concrete quality, loads M_d and/or N_d and the ratio As_2/As_1 are given.

Afterwards the results are depicted in a plot (fig. 18).

For a small ratio M_d/N_d see section HINTS AND WARNINGS (page 4).

Calculations are carried out on the basis of EUROCODE 2 (DIN EN 1992-1-1:2011-01) [1] and the accompanying national annex for Germany [2].

The consideration of the net area $A_{c,net}$ in the compressive area ($A_{c,comp} = x * b$) is optional, if $As_2 > 0$: $A_{c,net} = A_{c,comp} - As_2$

Quality of reinforcement: BSt 500 S (A) .

Allowed quality of concrete f_{ck} : C 12/15 - C 50/60, where the first number stands for the strength f_{ck} and the second one for $f_{ck,cube}$

Allowed ratio of reinforcement As_2/As_1 : $0 \leq As_2/As_1 \leq 1$

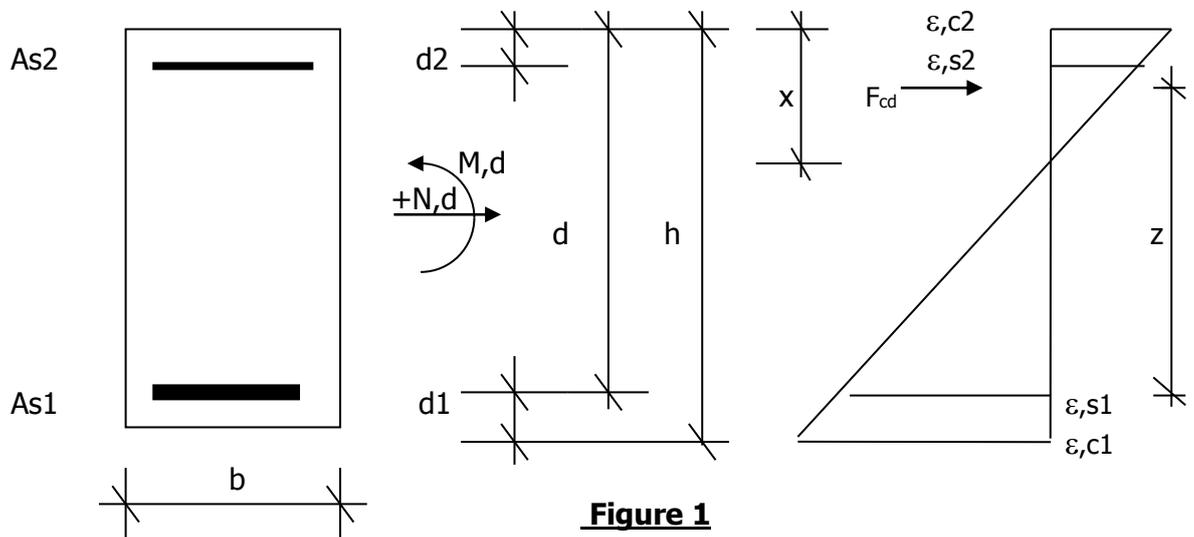


Figure 1

Taken into consideration is the distribution of concrete stress based on the „Parabel-Rechteck-Diagramm (P-R)“ (index **3**, default value), bilinear distribution (**2**) or block form of stress (**1**) (figures 3.3 – 3.5 of [1]).

As well as $f_{tk,cal} = 525 \text{ N/mm}^2$ and the simplified assumption $f_{tk,cal} = 500 \text{ N/mm}^2$ according to [1], fig. 3.8 for the relation of stress-strain of steel are provided.

INSTALLATION:

Store the file „Regbem“ in the MyLib-folder and start „regbem()“ on page 1.1 of the document.

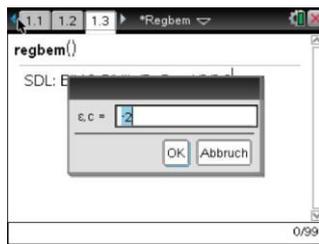
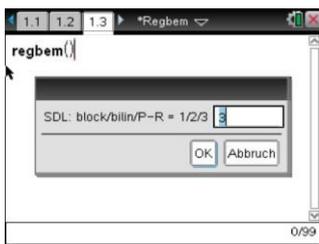
DESCRIPTION (explained in form of the following example) :

A rectangular concrete beam having a concrete quality of C30/37 with dimensions $b / h = 35 / 55$ cm and the distances of the layers of reinforcement $d_2 / d_1 = 5 / 5.5$ cm is reinforced with **3** bars diameter #**14** ($A_{s2} = 4.62 \text{ cm}^2$) on the top and **4** bars diameter #**25** ($A_{s1} = 19.63 \text{ cm}^2$) at the bottom.

Will the selected reinforcement be sufficient for the loads of $M_d = 387 \text{ kNm}$ and $N_d = -58 \text{ kN}$ (pressure force)?

Taken into account are the „Parabel-Rechteck-Diagramm (P-R) “ with $\epsilon_{s,c2} = -2\text{‰}$ and a steel stress of $f_{tk,cal} = 525 \text{ N/mm}^2$. The net area of the compressive zone is not to be considered.

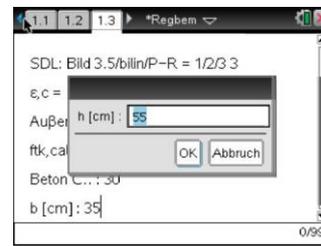
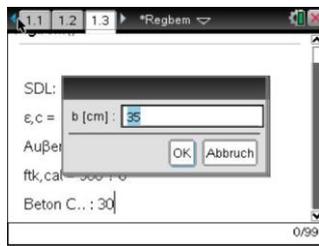
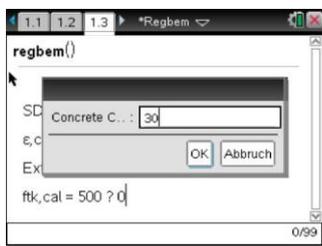
Select **regbem()** from the **var**-menu and enter the appropriate index for the used diagram concerning the distribution of concrete stress (Default: **3**, which will be the right value for this example), see fig. 2). Then use the default for $\epsilon_{s,c2}$ (= **-2‰**) as input (or enter $\epsilon_{s,c2}$) (fig. 3).



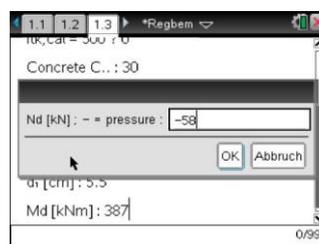
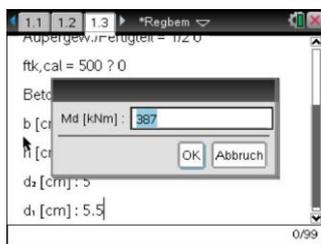
In the next screen (fig. 4) you may enter **1** for an extraordinary loadcase or **2** if a pre-fabricated beam is examined. That will change the normal safety factors ($\gamma_c = 1.5, \gamma_s = 1.15$) to $\gamma_c = 1.3, \gamma_s = 1.0$ or $\gamma_c = 1.35, \gamma_s = 1.15$, respectively. As this example handles a "normal" situation, leave the default value **0** (or enter it) in the input box.

Just do so in the following request: enter (or leave as default value) **0** for $f_{tk,cal} = 525 \text{ N/mm}^2$, otherwise key in **1** for " $\sigma=500$ ".

In the next request enter the quality in form of strength f_{ck} of the concrete "C..". (optional: 12, 16, 20, 25, 30, 35, 40, 45, 50), in this example key in **30**. (fig. 5)



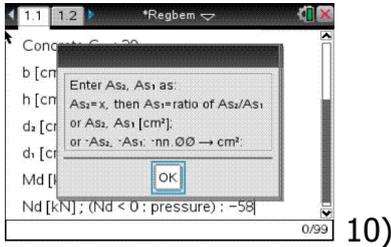
In the following screen enter **35** for b , **55** as value for h (fig. 6 - 7), then **5** and **5.5** for d_2 and d_1



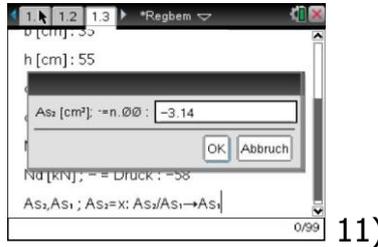
Now key in **387** for M_d (fig. 8) and **-58** for N_d (fig. 9). Be sure to use (-) as minus-key !

To enter the ratio A_{s2}/A_{s1} there are three options available (fig. 10):

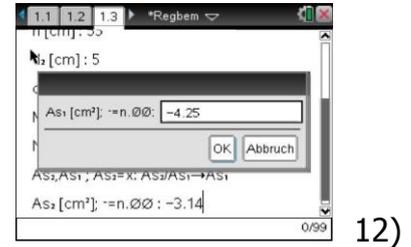
- (1) You enter a default ratio \rightarrow key in **x** for A_{s2} and the ratio **A_{s2}/A_{s1} (≤ 1 !)** in A_{s1} .
- (2) Enter an area [cm²] for A_{s2} and do so for A_{s1} . (Make sure that **$0 \leq A_{s2} \leq A_{s1}$!!!**)
- (3) Enter a **negative** value in form of **$-nn.dd$** , where **nn** is the number and **dd** the diameter # [mm] of bars.



10)



11)



12)

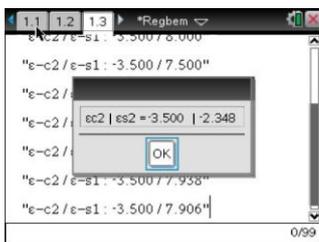
In our example enter **-3.14** in A_{s2} and **-4.25** in A_{s1} (fig. 11 – 12). The ratio will be set to **$4.618/19.635 = 0.2352$** .

In the next prompt for the input of the net area $A_{c,net}$ enter **0** (no consideration in this example), otherwise you would have to key in **1**.

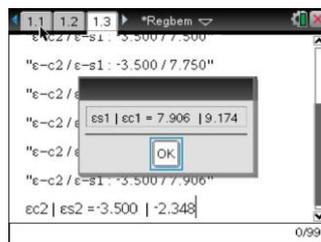
After some seconds of iteration the results are presented in text-boxes (fig. 13 – 17) in the following order (for the meaning of $\epsilon...$, x , z see pict. 1, press **ENTER** to continue the output:

$$\begin{aligned} \epsilon_{c2} / \epsilon_{s2} &= -3.500 / -2.348 \\ \epsilon_{s1} / \epsilon_{c1} &= 7.906 / 9.174 \\ \xi / x &= 0.307 / 15.2 \\ \zeta / z &= 0.872 / 43.2 \\ A_{s2} / A_{s1,req} &= 4.61 / 19.58 \text{ [cm}^2\text{]} \end{aligned}$$

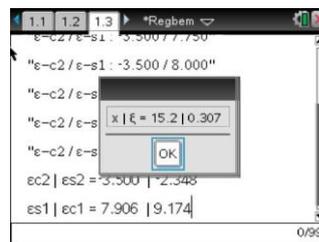
with :
 x : width of compression zone $\xi * d$ in [cm]
 z : width of internal lever $\zeta * d$ [cm], see pict. 1)



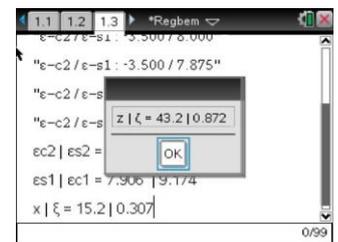
13)



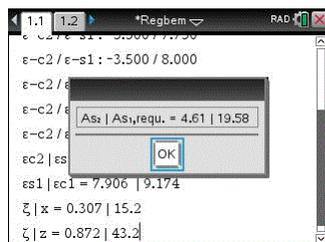
14)



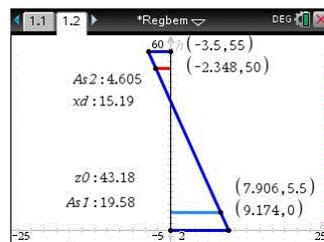
15)



16)



17)



18)

As the required reinforcement $A_{s1,requ}$ is less than the chosen area (19.63), the reinforcement of the beam is sufficient ($A_{s2,requ} \approx A_{s2,chosen}$!)

If $A_{s2} = 0$, the output of ϵ_{s2} and A_{s2} is omitted. Therefore, if you run the example again with A_{s2} being 0 (enter **x** for A_{s2} and **0** for A_{s1} according to option (1) above), the result will be:
 $A_{s1,requ} = 20.91 \text{ [cm}^2\text{]}$,

which is greater than the set area of 4 bars # 25 (19.63 cm²) for the bottom layer !

On page 1.2 you will find a plot showing the distribution of strains along the height (ε [%], h [cm]), the required reinforcement A_{s2} , $A_{s1,req}$ and the values for x and z (depicted as x_d and z_0), see fig. 18).

HINTS AND WARNINGS:

The form of the output of the recent version may slightly differ from the figures of that documentation!

If there is no solution possible, an appropriate warning will be issued.

This may be in the following cases:

$M/(|N| * h) \sim 0$ and $|N| < (b * h * 0.85 * f_{ck} / 1.5)$, if $N < 0$

Minimum reinforcement according to section 9.5.2 (2) of [1] and [2] is not taken into account.

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VERSION:

Vers. 1.0: first version submitted to the file archive

Vers. 2.0: plot of results added

Vers. 2.1: plot improved, some changes in the documentation

Vers. 2.5: plot revised

LITERATURE:

[1]: DIN EN 1992-1-1:2004 + AC 2010 (EUROCODE 2)

[2]: National Appendix DIN EN 1992-1-1/NA on the base of [1]

[3]: Wommelsdorff/Albert "Stahlbetonbau Teil 1 ; 10th edition (Werner publisher's)

[4]: Deutscher Ausschuss für Stahlbeton – Heft 525 "Erläuterungen zu DIN 1045-1"
2nd edition (Beuth publisher's)

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